

May 2008

# FAN5110 — Two-Phase, Bootstrapped, 12V NMOSFET Half-Bridge Driver

#### **Features**

- Two-phase, N-channel MOSFET driver in a Single Compact Package for Multi-phase Buck Converter **Applications**
- Each Phase Drives the N-channel High-side and Low-side MOSFETs in a Synchronous Buck Configuration
- Two-phase Driver Reduces Printed Circuit Board Area
- Variable High-side and Low-side Gate Drive Voltages for Flexibility and Performance Optimization at **Higher Frequencies**
- Internal Adaptive "Shoot-through" Protection
- Fast Rise and Fall Times
- High Switching Frequency: up to 1 MHz
- Common Enable (EN) Turns Off both Upper and Lower Output FETs
- TTL-compatible PWM and EN Inputs
- Under-Voltage Lockout Protection Feature
- Available in SOIC-16 and MLP-16 Packages

### **Applications**

- Multi-Phase VRM/VRD Regulators for Microprocessor Supplies
- Two Separate, Single-phase Supply Designs
- High-Current, High-Frequency DC/DC Converters
- High-Power Modular Supplies
- General-Purpose, TTL Input, 12V Driver for Half-Bridge and Full-Bridge Applications

### **Description**

FAN5110 contains two N-channel MOSFET drivers on a single die in one package. It replaces two single-phase drivers in a multiple-phase PWM design. Each phase is specifically designed to drive both the upper and lower N-channel power MOSFETs of a synchronous rectified buck converter at high switching frequencies.

This two-phase driver, combined with a Fairchild multiphase PWM controller and power MOSFETs, forms a complete V-core power supply solution for advanced microprocessors.

The lower drivers are powered externally through the PVCC pin. The PVCC pin is normally connected to V<sub>CC</sub>, which drives the lower MOSFET's gates at 12VGS. Connecting the PVCC pin to a voltage lower than V<sub>CC</sub> lowers the V<sub>GS</sub> voltage, resulting in much less driver power dissipation. This is especially valuable when driving MOSFETs with high gate charge (Qotot) and in applications requiring high switching frequencies.

The driver's adaptive shoot-through protection prevents the upper and lower MOSFETs from conducting simultaneously. The FAN5110 is rated for operation from 0°C to +85°C and is available in a low-cost 16-pin (Small Outline Integrated Circuit) SOIC package and a higher power MLP-16 package.

#### **Related Resources**

 AN-6003 — "Shoot-through" in Synchronous **Buck Converters** 

# **Ordering Information**

Part Number	Operating Temperature Range	Package	© Eco Status	Packing Method	Quantity Per Reel
FAN5110MX	0°C to 85°C	SOIC-16	RoHS	Tape and Reel	2500
FAN5110MPX	0°C to 85°C	MLP-16, 4x4mm	RoHS	Tape and Reel	2500

For Fairchild's definition of "green" Eco Status, please visit: <a href="http://www.fairchildsemi.com/company/green/rohs\_green.html">http://www.fairchildsemi.com/company/green/rohs\_green.html</a>.

# **Pin Configurations**

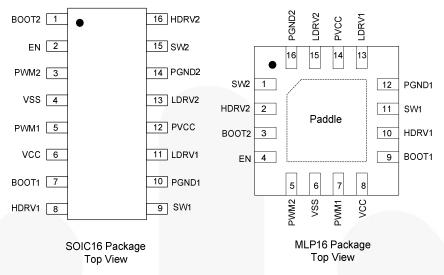


Figure 1. Packages (Top View)

# **Pin Definitions**

MLP	SOIC	Name	Description					
1	15	SW2	<b>Switch Node Input</b> . Connect as shown in Figure 1. SW provides return for the high-side bootstrapped driver and acts as a sense point for the adaptive shoot-through protection.					
2	16	HDRV2	High-Side Gate Drive Output. Connect to the gate of the high-side power MOSFET(s).					
3	1	воот2	<b>Bootstrap Supply Input</b> . Provides voltage supply to the high-side MOSFET driver. Connect to bootstrap capacitor and diode.					
4	2	EN	<b>Enable</b> . When LOW, this pin disables FET switching (HDRV and LDRV are held LOW). This pin is common for both drivers (previously referred to as OD#).					
5	3	PWM2	PWM Signal Input. Accepts a logic-level PWM signal from the controller.					
6	4	vss	Signal Ground. Connect directly to the ground plane.					
7	5	PWM1	PWM Signal Input. Accepts a logic-level PWM signal from the controller.					
8	6	vcc	<b>ower Input Voltage</b> . +12V power for the internal logic. Bypass with a minimum 1μF 7R or 4.7μF X5R ceramic capacitor.					
9	7	BOOT1	<b>Bootstrap Supply Input</b> . Provides voltage supply to the high-side MOSFET driver. Connect to bootstrap capacitor and diode.					
10	8	HDRV1	High Gate Drive Output. Connect to the gate of the high-side power MOSFET(s).					
11	9	SW1	<b>Switch Node Input</b> . Connect as shown in Figure 1. SW provides return for the high-side bootstrapped driver and acts as a sense point for the adaptive shoot-through protection.					
12	10	PGND1	Power Ground. Connect directly to the source of low-side MOSFET(s) and C <sub>VCC</sub> .					
13	11	LDRV1	Low-Side Gate Drive Output. Connect to the gate of the low-side power MOSFET(s).					
14	12	PVCC	<b>Lower Gate Drive Voltage</b> . This is the input supply for the lower drivers. The $V_{GS}$ of the lower MOSFETs matches this voltage. Connect to $V_{CC}$ or a lower voltage.					
15	13	LDRV2	Lower Gate Drive Output. Connect to the gate of the low-side power MOSFET(s).					
16	14	PGND2	Power Ground. Connect directly to the source of low-side MOSFET(s) and C <sub>VCC</sub> .					
	NA	Paddle	<b>MLP Package Only.</b> Connected to ground inside the chip. Connect to ground plane for lowest thermal resistance.					

# **Application Diagram**

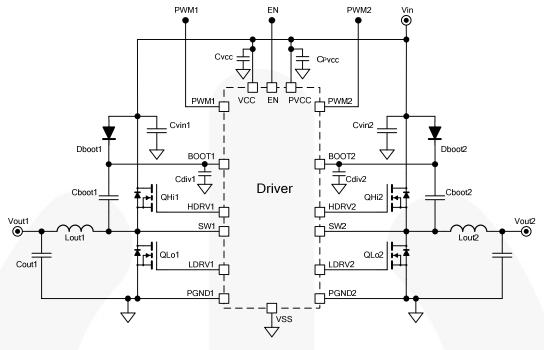


Figure 2. Typical Two-Phase Application

# **Block Diagram**

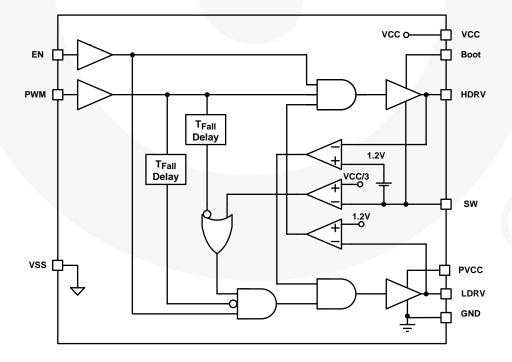


Figure 3. Functional Block Diagram, Each Side

## **Absolute Maximum Ratings**

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. Absolute maximum ratings are stress ratings only. Unless otherwise specified, voltages referenced to GND.

Parameter	Conditions	Min.	Max.	Unit
VCC and PVCC to GND	Continuous	-0.3	15.0	V
VCC and PVCC to GND	Transient (t < 4ns) <sup>(1)</sup>	-0.3	19.0	V
PWM and EN Pins		-0.3	5.5	V
SW to CND	Continuous	-1	15	V
SW to GND	Transient (t < 100ns) <sup>(1)</sup>	-5	25	V
BOOT to SW	Continuous	-0.3	15.0	V
BOOT 10 SW	Transient (t < 20ns)	-2	17	V
DOOT to CND	Continuous	-0.3	30.0	V
BOOT to GND	Transient (t < 100ns) <sup>(1)</sup>		38	V
HDRV		V <sub>SW</sub> -1.0	V <sub>BOOT</sub> +0.3	V
	Continuous	-0.5	V <sub>CC</sub>	V
LDRV	Transient (t < 200ns) <sup>(1)</sup>	-2.0	V <sub>CC</sub> +0.3	V
	Transient (t < 20ns)	-2.0	V <sub>CC</sub> +2.0	V

#### Note:

### **Thermal Information**

Symbol	Parameter	Min.	Тур.	Max.	Unit
TJ	Junction Temperature	0		+150	°C
T <sub>STG</sub>	Storage Temperature	-65		+150	°C
TL	Lead Soldering Temperature, 10 Seconds			+300	°C
$T_VP$	Vapor Phase, 60 Seconds			+215	°C
T <sub>LI</sub>	Infrared, 15 Seconds			+220	°C
P <sub>D</sub>	Power Dissipation, T <sub>A</sub> = 25°C, T <sub>JMAX</sub> = 125°C		-/-	850	mW
$\theta_{JC}$	Thermal Resistance, SO-16, Junction-to-Board		40		°C/W
$\theta_{JA}$	Thermal Resistance, SO-16, Junction-to-Ambient		117	y	°C/W
θ <sub>JC</sub>	Thermal Resistance, MLP16, Junction-to-Case		5		°C/W
$\theta_{JA}$	Thermal Resistance, MLP16, Junction-to-Ambient		37		°C/W

### **Recommended Operating Conditions**

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended operating conditions are specified to ensure optimal performance to the datasheet specifications. Fairchild does not recommend exceeding them or designing to Absolute Maximum Ratings.

Symbol	Parameter	Conditions	Min.	Тур.	Max.	Unit
Vcc	Supply Voltage	V <sub>CC</sub> to Ground	10.0	12.0	13.5	٧
PVcc	PVCC Input Voltage	PV <sub>CC</sub> to Ground	8.0	12.0	13.5	V
V <sub>IO</sub>	Boot Diode Anode Voltage	Anode to Ground	8.0	12.0	13.5	V
T <sub>A</sub>	Ambient Temperature		0		+85	°C
TJ	Junction Temperature		0		+125	°C

<sup>1.</sup> For transient derating beyond the levels indicated, refer to Figure 17 and Figure 18.

### **Electrical Characteristics**

 $V_{\text{CC}}$  and  $P_{\text{VCC}}$  = 12V, and  $T_{\text{A}}$  = 25°C using the circuit in Figure 4 unless otherwise noted. The "•" denotes specifications that apply over the full operating temperature range.

Symbol	Parameter	Conditions		Min.	Тур.	Max.	Unit
Input Supply			,			1	
V <sub>CC</sub>	V <sub>CC</sub> and P <sub>VCC</sub> Voltage Range		•	6.4	12.0	13.5	V
I <sub>CC</sub>	V <sub>CC</sub> Current	EN = 0V	•		4.1	8.0	mA
$V_{UYR}$	V <sub>CC</sub> Rising	1V/ms			4.7	5.3	V
$V_{UVF}$	V <sub>CC</sub> Falling	1V/ms		3.4	4.2		V
V <sub>HYS</sub>	V <sub>CC</sub> Hysteresis			175	325		mV
EN Input							
V <sub>IH(EN)</sub>	Input High Voltage		•	2.0			V
V <sub>IL(EN)</sub>	Input Low Voltage		•			0.8	V
V <sub>HYS(EN)</sub>	Input Hysteresis		•		550		mV
I <sub>EN</sub>	Input Current	EN = 3.0V	•	-300		+300	nA
t <sub>pdl(EN)</sub>	D. (3)	Figure 5			25	40	ns
t <sub>pdh(EN)</sub>	Propagation Delay <sup>(3)</sup>				15	30	ns
PWM Input						•	
$V_{\text{IH}(\text{PWM})}$	Input High Voltage		•	2.0			V
$V_{\text{IL}(\text{PWM})}$	Input Low Voltage		•			0.8	V
V <sub>HYS(PWM)</sub>	Input Hysteresis		•		550		mV
I <sub>IL(PWM)</sub>	Input Current		•	-1		+1	μA
SW Pin							
R <sub>SW</sub>	SW Pin Bleeder	EN = 0V, V <sub>SW</sub> = 4.0V	•	700	1000	1300	Ω
High-Side Dr	iver					•	
R <sub>HUP</sub>	Output Resistance, Sourcing	$V_{BOOT} - V_{SW} = 12V$			2.5	3.3	Ω
I <sub>SOURCE(LDRV)</sub>	Source Current <sup>(3)</sup>	V <sub>DS</sub> = -10V			2.0		Α
R <sub>HDN</sub>	Output Resistance, Sinking	$V_{BOOT} - V_{SW} = 12V$			1.1	1.4	Ω
I <sub>SINK(HDRV)</sub>	Sink Current <sup>(3)</sup>	V <sub>DS</sub> = 10V			2.7		Α
t <sub>R(HDRV)</sub>	T(3, 5)				30	45	ns
t <sub>F(HDRV)</sub>	Transition Times <sup>(3, 5)</sup>	Figure 4			25	30	ns
$t_{\text{pdh(HDRV)}}$	D (3.4)	E: 0			35	50	ns
t <sub>pdl(HDRV)</sub>	Propagation Delay <sup>(3, 4)</sup>	Figure 6			25	40	ns

Continued on the following page...

### **Electrical Characteristics** (Continued)

 $V_{\text{CC}}$  and  $P_{\text{VCC}}$  = 12V, and  $T_{\text{A}}$  = 25°C using the circuit in Figure 4 unless otherwise noted. The "•" denotes specifications that apply over the full operating temperature range.

Symbol	Parameter	Conditions		Min.	Тур.	Max.	Unit	
Low-Side Dri	Low-Side Driver							
PVCC	PVCC Voltage Range			6.4	12.0	13.5	V	
R <sub>LUP</sub>	Output Resistance, Sourcing				2.0	2.3	Ω	
I <sub>SOURCE(LDRV)</sub>	Source Current <sup>(3)</sup>	V <sub>DS</sub> = -10V			2.7		Α	
R <sub>LDN</sub>	Output Resistance, Sinking				1.0	1.3	Ω	
I <sub>SINK(LDRV)</sub>	Sink Current <sup>(3)</sup>	V <sub>DS</sub> = 10V			3.5		Α	
BG <sub>th</sub>	Bottom Gate Threshold			1.0	1.3	1.6	٧	
BG <sub>hys</sub>	Bottom Gate Hysteresis			0.5	0.8		<b>V</b>	
t <sub>R(LDRV)</sub>	Transition Times <sup>(3, 5)</sup>	Figure 4			25	35	ns	
t <sub>F(LDRV)</sub>	Transition filles	Figure 4			20	30	ns	
t <sub>pdh(LDRV)</sub>		Figure 6			20	30	ns	
$t_{pdl(LDRV)}$	Propagation Delay <sup>(3, 4)</sup>	Figure 6			15	20	ns	
$t_{pdh(LDF)}$	, 3	See Adaptive Gate Drive Circuit Description			170		ns	

#### Notes

- 2. Limits at operating temperature extremes are guaranteed by design, characterization, and statistical quality control.
- 3. Specifications guaranteed by design and characterization (not production tested).
- 4. For propagation delays, t<sub>pdh</sub> refers to low-to-high signal transition. t<sub>pdl</sub> refers to high-to-low signal transition.
- 5. Transition times are defined for 10% and 90% of DC values.

# **Test Diagrams**

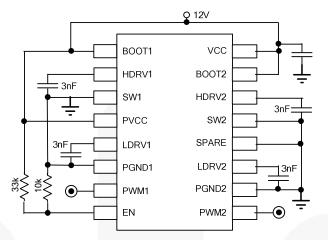


Figure 4. Test Circuit

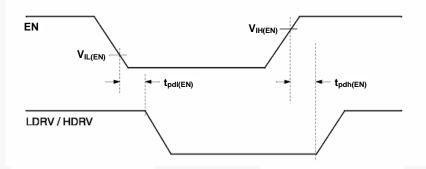


Figure 5. Enable Timing

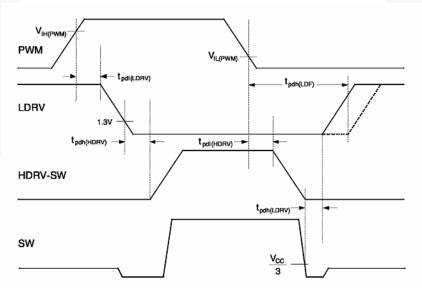


Figure 6. Adaptive Gate Drive Timing

# **Typical Performance Characteristics**

Performance characteristics achieved using the test circuit shown in Figure 4.

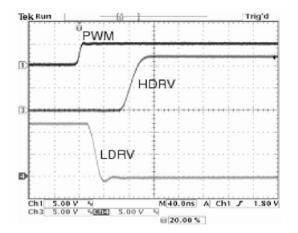


Figure 7. PWM Rise Time Waveforms

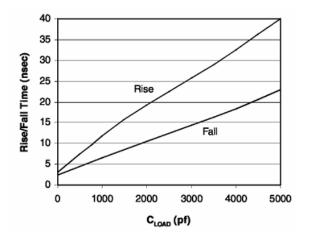


Figure 9. HDRV Rise and Fall Times vs. CLOAD

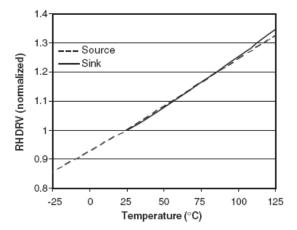


Figure 11. HDRV Resistance vs. Temperature

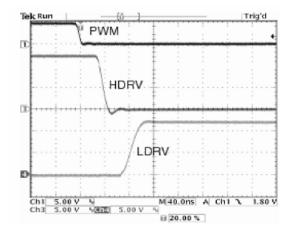


Figure 8. PWM Fall Time Waveforms

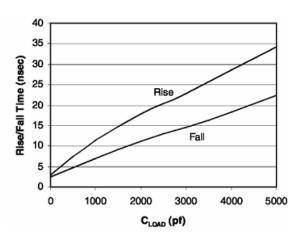


Figure 10. LDRV Rise and Fall Times vs. CLOAD

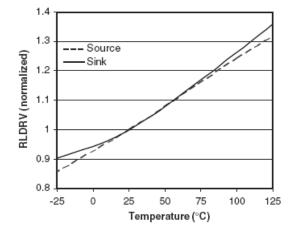


Figure 12. LDRV Resistance vs. Temperature

# **Typical Performance Characteristics** (Continued)

Performance characteristics achieved using the test circuit shown in Figure 4.

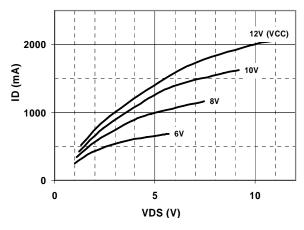


Figure 13. HDRV Pull-Up (Sourcing)

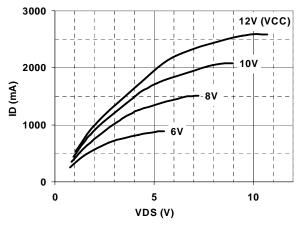


Figure 14. LDRV Pull-Up (Sourcing)

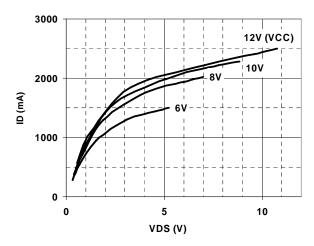


Figure 15. HDRV Pull-Down (Sinking)

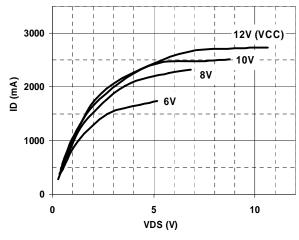


Figure 16. LDRV Pull-Down (Sinking)

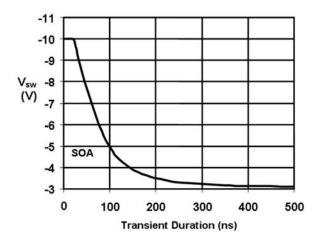


Figure 17. Negative SW Voltage Transient

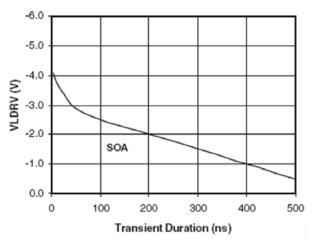


Figure 18. Negative LDRV Voltage Transient

### **Typical Performance Characteristics** (Continued)

Performance characteristics below were achieved using a modified version of the test circuit shown in Figure 4. The BOOT and PVCC pins were disconnected from  $V_{CC}$ ; a boot diode was connected in series with the BOOT pin; and the PVCC and boot diode anode were connected to a variable voltage power supply.  $V_{CC}$  was held constant at 12V during the test.

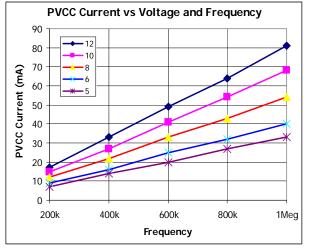


Figure 19. PV<sub>CC</sub> Operating Current

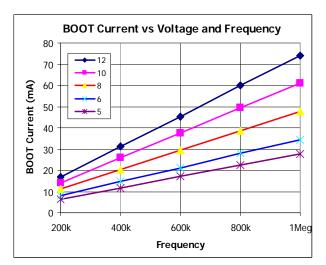


Figure 20. Boot Operating Current

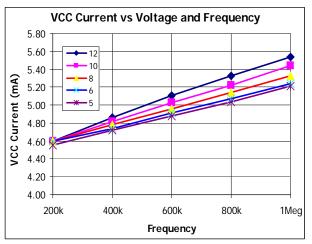


Figure 21. V<sub>CC</sub> Operating Current

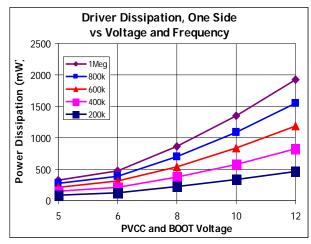


Figure 22. Driver Power Dissipation, One Side

### **Circuit Description**

The FAN5110 contains two half-bridge MOSFET drivers in a single 16-pin package. Each driver is optimized for driving N-channel MOSFETs in a synchronous buck converter topology. Each driver's TTL-compatible PWM input signal is all that is required to properly drive the high-side and low-side MOSFETs. The following sections apply to each driver.

#### **Low-Side Driver**

The low-side driver (LDRV) is designed to drive ground-referenced, low- $R_{DS(on)}$ , N-channel MOSFETs. The power for LDRV is internally connected to the PVCC pin. When the driver is enabled, the driver's output is 180° out of phase with the PWM input. When the FAN5110 is disabled (EN = 0V), LDRV is held low.

#### **High-Side Driver**

The FAN5110's high-side driver (HDRV) is designed to drive a floating N-channel MOSFET. The bias voltage for the high-side driver is developed by a bootstrap supply circuit, consisting of an external diode and bootstrap capacitor ( $C_{BOOT}$ ).

During start-up, SW is held at GND, allowing  $C_{\text{BOOT}}$  to charge to  $V_{\text{CC}}$  through the diode. When the PWM input goes high, HDRV begins to charge the high-side MOSFET gate (QHi). During this transition, charge is transferred from  $C_{\text{BOOT}}$  to QHi's gate. As QHi turns on, SW rises to  $V_{\text{IN}}$ , forcing the BOOT pin to  $V_{\text{IN}}$  +  $V_{\text{C(BOOT)}}$ , which provides sufficient  $V_{\text{GS}}$  enhancement for QHi. To complete the switching cycle, QHi is turned off by pulling HDRV to SW.  $C_{\text{BOOT}}$  is recharged to  $V_{\text{CC}}$  when SW falls to GND. HDRV output is in phase with PWM input. When the driver is disabled, the high-side gate is held low.

#### **Adaptive Gate Drive Circuit**

The FAN5110 embodies an advanced design that ensures minimum MOSFET dead-time, while eliminating potential shoot-through (cross-conduction) currents. It senses the state of the MOSFETs and adjusts the gate drive, adaptively, to ensure they do not conduct simultaneously. Refer to the gate drive rise and fall time waveforms shown in Figure 7 and Figure 8 for the relevant timing information.

To prevent overlap during the low-to-high switching transition (QLo OFF to QLo ON), the adaptive circuitry monitors the voltage at the LDRV pin. When the PWM signal goes HIGH, QHi begins to turn OFF after a propagation delay, as defined by the  $t_{\text{pdl}(\text{LDRV})}$  parameter. Once the LDRV pin is discharged below ~1.3V, QHi begins to turn ON after adaptive delay  $t_{\text{pdh}(\text{HDRV})}$ .

To preclude overlap during the high-to-low transition (QLo OFF to QHi ON), the adaptive circuitry monitors the voltage at the SW pin. When the PWM signal goes LOW, QLo begins to turn OFF after a propagation delay ( $t_{pdl(HDRV)}$ ). Once the SW pin falls below  $V_{CC}/3$ , QHi begins to turn ON after adaptive delay  $t_{pdh(LDRV)}$ .

 $V_{GS}$  of QLo is also monitored. When  $V_{GS(QLo)}$  is discharged below ~1.3V, a secondary adaptive delay is initiated, which results in QHi being driven ON after  $t_{pdh(LDF)}$ , regardless of the SW state. This function is implemented to ensure that  $C_{BOOT}$  is recharged after each switching cycle, particularly for cases where the power converter is sinking current and the SW voltage does not fall below the  $V_{CC}/3$  adaptive threshold. The secondary delay  $t_{pdh(LDF)}$  is longer than  $t_{pdh(LDRV)}$ .

### **Application Information**

#### **Supply Capacitor Selection**

For the supply input ( $V_{CC}$ ), a local ceramic bypass capacitor is recommended to reduce the noise and to supply the peak current. Use at least a 1 $\mu$ F, X7R or X5R capacitor, close to the VCC and PGND pins. A 1 $\mu$ F bypass capacitor should be connected at the PVCC pin to PGND.

### **Bootstrap Circuit**

The bootstrap circuit uses a charge storage capacitor  $(C_{BOOT})$  and an external diode, as shown in Figure 2. These components should be selected after the high-side MOSFET has been chosen. The required capacitance is determined using the following equation:

$$C_{\text{BOOT}} = \frac{Q_{\text{G}}}{\Delta V_{\text{BOOT}}} \tag{1}$$

where  $Q_{\rm G}$  is the total gate charge of the high-side MOSFET and  $\Delta V_{BOOT}$  is the voltage droop allowed on the high-side MOSFET drive. For example, the  $Q_{\rm G}$  of the FDD6696 MOSFET is about 35nC at 12V\_Gs. For an allowed droop of ~300mV, the required bootstrap capacitance is 100nF. A good quality ceramic capacitor must be used.

The average diode forward current,  $I_{\text{F(AVG)}}$ , can be estimated by:

$$I_{f(AVG)} = Q_{GATE} \times f_{SW}$$
 (2)

where f<sub>SW</sub> is the switching frequency of the controller.

The peak surge current rating of the diode should be checked in-circuit, since this is dependent on the equivalent impedance of the entire bootstrap circuit, including the PCB traces.

#### **Thermal Considerations**

The total device dissipation is the total of both phases.

Device dissipation for a phase can be calculated as:

$$P_{Dtot} = P_{Q} + P_{HDRV} + P_{LDRV}$$
 (3)

where:

Po represents quiescent power dissipation:

$$P_Q = V_{CC} \times [4mA + 0.036(f_{SW} - 100)]$$
 (4)

f<sub>SW</sub> is switching frequency (in kHz).

 $P_{\mbox{\scriptsize HDRV}}$  represents the power dissipation of the upper FET driver.

PLDRV is dissipation of the lower FET driver.

#### Calculation of PHDRV:

$$P_{QH} = \frac{1}{2} \times Q_{GH} \times V_{GS(Q1)} \times f_{SW}$$
 (5)

$$P_{HDRV} = P_{H(R)} + P_{H(F)}$$
 (6)

$$P_{H(R)} = P_{QH} \times \frac{R_{HUP}}{R_{HUP} + R_F + R_G}$$
 (7)

$$P_{H(F)} = P_{QH} \times \frac{R_{HDN}}{R_{HUP} + R_F + R_G}$$
 (8)

where:

 $P_{H(R)}$  and  $P_{H(F)}$  are dissipations for the rising and falling edges, respectively.

 $Q_{GH}$  is total gate charge of the upper FET for its applied  $V_{\text{GS}}.$ 

As described in Equations 6 and 7, the total power dissapated in driving the gate is divided in proportion to the resistances in series with the MOSFET internal gate node, as shown in Figure 23.

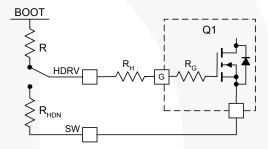


Figure 23. Driver Dissipation Model

 $R_G$  is the gate resistance internal to the FET.  $R_E$  is the external gate drive resistor implemented in many designs. Note that the introduction of  $R_E$  can reduce driver power dissipation, but excess  $R_E$  may cause errors in the "adaptive gate drive" circuitry. In particular, adding  $R_E$  in the low drive circuit could result in shoot-through. For more information, refer to *Application Note AN-6003*, "Shoot-through" in Synchronous Buck Converters.

#### Calculation of PLDRV:

$$P_{OH} = \frac{1}{2} \times Q_{GH} \times V_{GS(O1)} \times f_{SW}$$
(9)

$$P_{LDRV} = P_{L(R)} + P_{L(F)}$$
 (10)

$$P_{L(R)} = P_{QL} \times \frac{R_{LUP}}{R_{LUP} + R_E + R_G}$$
 (11)

$$P_{L(F)} = P_{QL} \times \frac{R_{LDN}}{R_{HDN} + R_F + R_G}$$
 (12)

where:

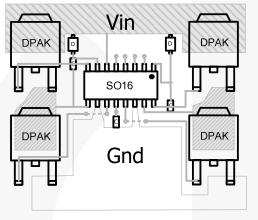
 $P_{L(R)}$  and  $P_{L(F)}$  are internal dissipations for the rising and falling edges, respectively.

 $Q_{\text{GL}}$  is total gate charge of the lower FET for its applied  $V_{\text{GS}}.$ 

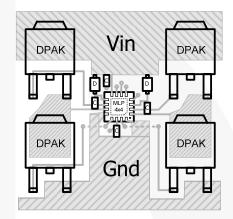
## **Layout Considerations**

Use the following general guidelines when designing printed circuit boards (see Figure 24):

- Trace out the high-current paths and use short, wide (>25 mil) traces to make these connections. If vias are required use multiple vias to lower the inductance.
- Connect the PGND pin as close as possible to the source of the lower MOSFET.
- The V<sub>CC</sub> bypass capacitor <u>must</u> be located as close as possible to the VCC and VSS pins of the device. This is also true for the PV<sub>CC</sub> bypass capacitor (PVCC and the PGND pins).
- Use multiple vias to other layers when possible to maximize the conduction of heat away from the package. This is particularly true for the paddle of the MLP package, which can be connected with vias to the internal ground plane of the board.







MLP16D Package

Figure 24. Recommended Layout Examples

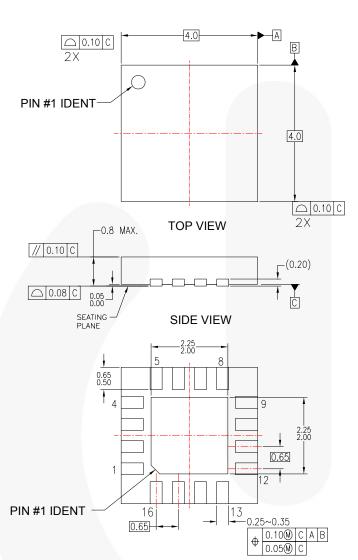
### **Physical Dimensions** 10.00 9.80 8.89 16 9 В 4.00 6.00 5.6 3.80 8 **PIN ONE INDICATOR** 0.65 0.35 (0.30)⊕ 0.25 M C B A LAND PATTERN RECOMMENDATION 1.75 MAX SEE DETAIL A 1.50 1.25 0.25 0.25 С 0.10 0.19 □ 0.10 C 0.50 0.25 X 45° NOTES: UNLESS OTHERWISE SPECIFIED (R0.10) A) THIS PACKAGE CONFORMS TO JEDEC MS-012, VARIATION AC, ISSUE C. **GAGE PLANE** (R0.10)B) ALL DIMENSIONS ARE IN MILLIMETERS. C) DIMENSIONS ARE EXCLUSIVE OF BURRS, MOLD 0.36 FLASH AND TIE BAR PROTRUSIONS CONFORMS TO ASME Y14.5M-1994 LANDPATTERN STANDARD: SOIC127P600X175-16AM F) DRAWING FILE NAME: M16AREV12. SEATING PLANE 0.90 0.50 (1.04)**DETAIL A** SCALE: 2:1

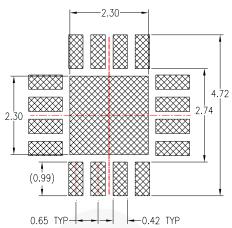
Figure 25. 16-Lead, Small Outline Integrated Circuit (SOIC) Package, 0.150 inches Narrow, JEDEC MS-012

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# **Physical Dimensions**





RECOMMENDED LAND PATTERN

NOTES: BOTTOM VIEW

A. CONFORMS TO JEDEC REGISTRATION MO-220, VARIATION WGGC, DATED MAY/2005

- B. DIMENSIONS ARE IN MILLIMETERS.
- C. DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994

#### MLP16DrevB

Figure 26. 16 Lead MLP, JEDEC MO-220, 4mm Square

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Rev. 134

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